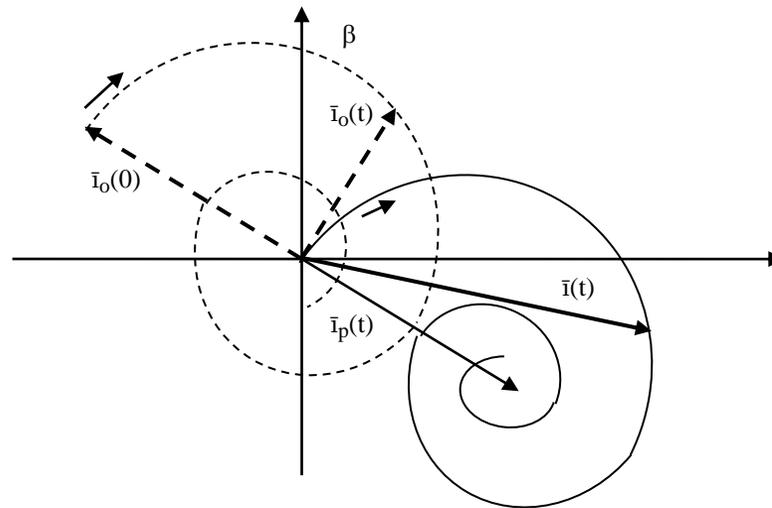


Electric Drives  
Laboratory  
DII - UniPD

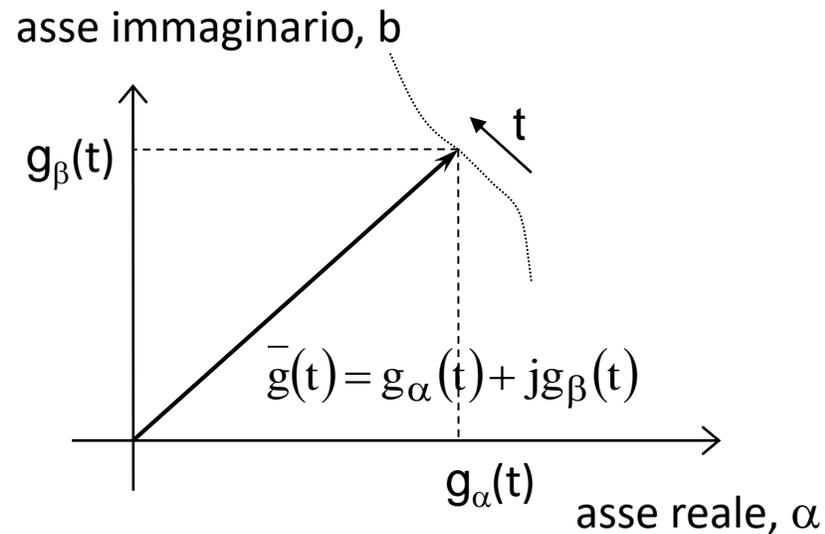
# Azionamenti Elettrici

Slides delle lezioni  
prof. Silverio Bolognani

# Vettori spaziali



## Vettore spaziale - definizione



$$\bar{g}(t) = \frac{2}{3} [g_a(t) + g_b(t)e^{j2\pi/3} + g_c(t)e^{j4\pi/3}] = g_\alpha(t) + j g_\beta(t)$$

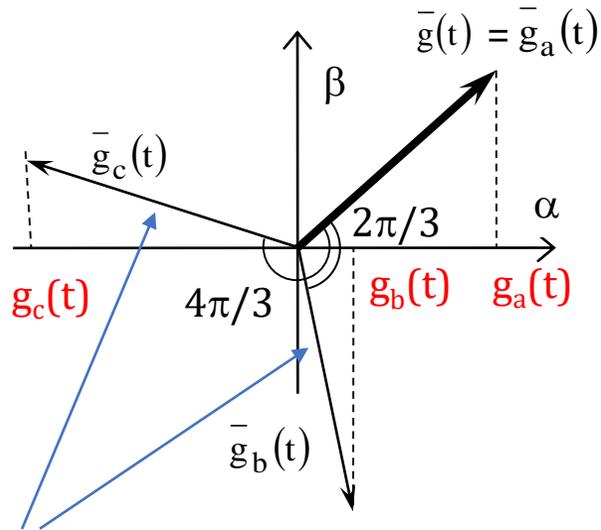
$$\text{Re}[\bar{g}(t)] = g_\alpha(t) = \frac{2}{3} \left[ g_a(t) - \frac{g_b(t)}{2} - \frac{g_c(t)}{2} \right]$$

$$\text{Im}[\bar{g}(t)] = g_\beta(t) = \frac{2}{3} \left[ g_b(t) \frac{\sqrt{3}}{2} - g_c(t) \frac{\sqrt{3}}{2} \right] = \frac{1}{\sqrt{3}} [g_b(t) - g_c(t)]$$

Grandezza «**bi-dimensionale**» associata ad una terna di grandezze trifase di qualsiasi forma d'onda

## Vettore spaziale - terna bilanciata

$$g_o(t) = \frac{g_a(t) + g_b(t) + g_c(t)}{3} = 0$$



Riflessioni simmetriche: vettori ausiliari per esemplificare graficamente il calcolo di  $\bar{g}_b(t)$  e  $\bar{g}_c(t)$ .

$$Re[\bar{g}(t)] = g_\alpha(t) = g_a(t)$$

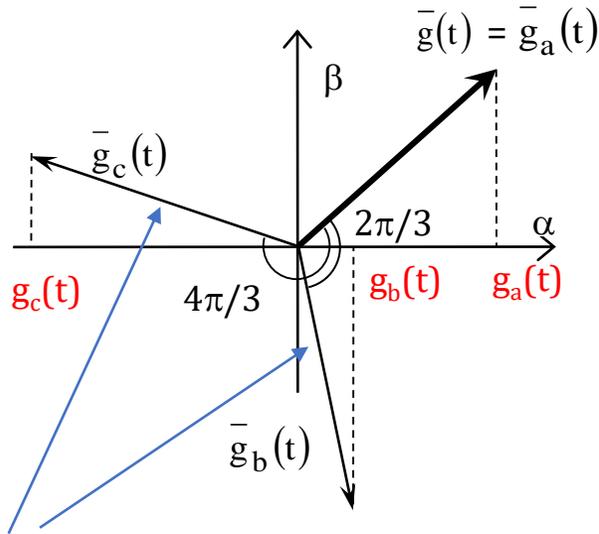
$$\bar{g}_b(t) = \bar{g}(t)e^{-j2\pi/3} = \frac{2}{3} [g_a(t)e^{-j2\pi/3} + g_b(t) + g_c(t)e^{j2\pi/3}]$$

$$Re[\bar{g}_b(t)] = Re[\bar{g}(t)e^{-j2\pi/3}] = -g_\alpha(t) \frac{1}{2} + g_\beta(t) \frac{\sqrt{3}}{2} = g_b(t)$$

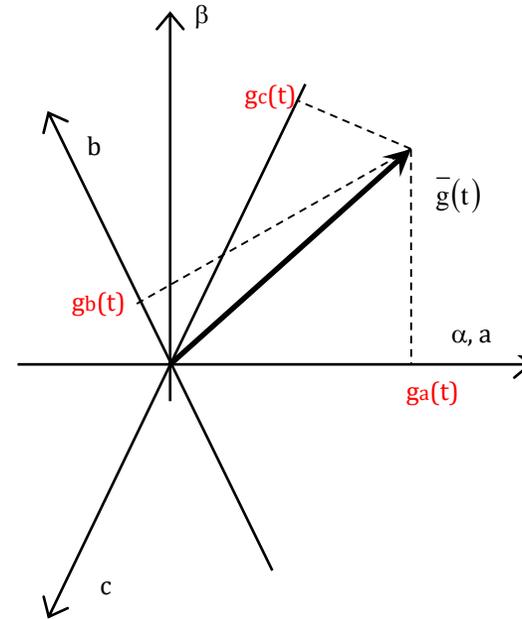
$$Re[\bar{g}_c(t)] = Re[\bar{g}(t)e^{-j4\pi/3}] = -g_\alpha(t) \frac{1}{2} - g_\beta(t) \frac{\sqrt{3}}{2} = g_c(t)$$

## Vettore spaziale – *terna bilanciata*

$$g_o(t) = \frac{g_a(t) + g_b(t) + g_c(t)}{3} = 0$$



Riflessioni simmetriche: vettori ausiliari per esemplificare graficamente il calcolo di  $\bar{g}_b(t)$  e  $\bar{g}_c(t)$ .



In alternativa alle proiezioni delle *Riflessioni simmetriche* sull'asse reale, si possono usare le proiezioni del vettore spaziale sugli assi  $b$  e  $c$ .

## Vettore spaziale – terna non bilanciata

$$g_o(t) = \frac{g_a(t) + g_b(t) + g_c(t)}{3} \neq 0$$

$$\left\{ \begin{array}{l} g_a(t) = g'_a(t) + g_o(t) \\ g_b(t) = g'_b(t) + g_o(t) \\ g_c(t) = g'_c(t) + g_o(t) \end{array} \right.$$

Si compone di una terna bilanciata e di una terna omopolare.

$$\begin{aligned} \bar{g}(t) &= \frac{2}{3} [g_a(t) + g_b(t)e^{j2\pi/3} + g_c(t)e^{j4\pi/3}] = \\ &= \frac{2}{3} [g'_a(t) + g'_b(t)e^{j2\pi/3} + g'_c(t)e^{j4\pi/3}] \end{aligned}$$

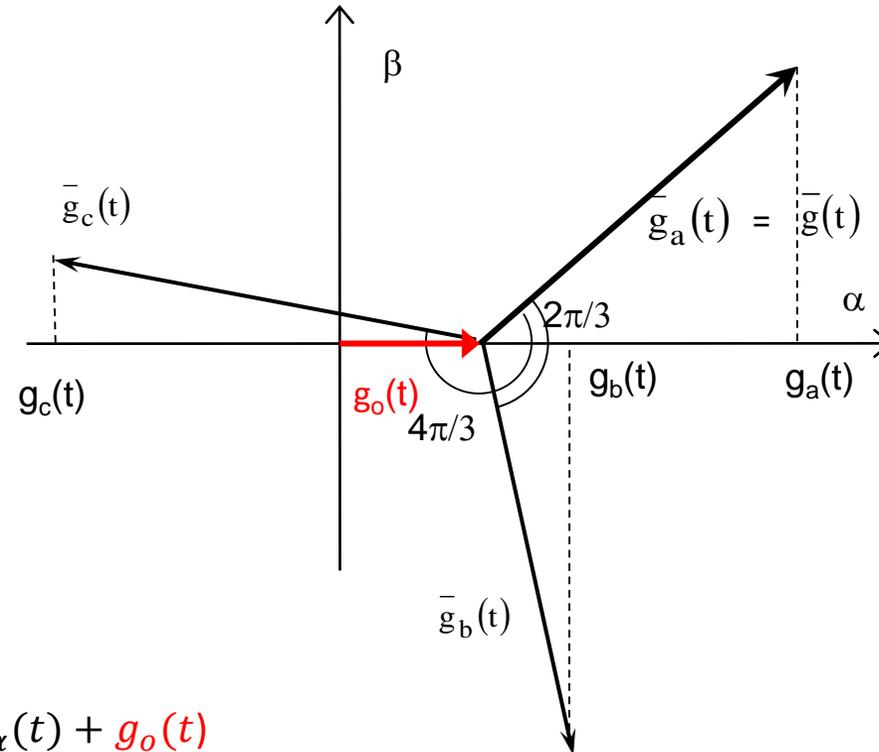
  $\bar{g}(t)$  non dipende dalla componente omopolare!

$$g_\alpha(t) = \frac{2}{3} \left[ g_a(t) - \frac{g_b(t)}{2} - \frac{g_c(t)}{2} \right]$$

$$g_\beta(t) = \frac{1}{\sqrt{3}} [g_b(t) - g_c(t)]$$

## Vettore spaziale – terna non bilanciata

$$g_o(t) = \frac{g_a(t) + g_b(t) + g_c(t)}{3} \neq 0$$



$$g_a(t) = \text{Re}[\bar{g}(t)] + g_o(t) = \text{Re}[\bar{g}_a(t)] + g_o(t) = g_\alpha(t) + g_o(t)$$

$$g_b(t) = \text{Re}[\bar{g}(t)e^{-j2\pi/3}] + g_o(t) = \text{Re}[\bar{g}_b(t)] + g_o(t) = -\frac{1}{2}g_\alpha(t) + \frac{\sqrt{3}}{2}g_\beta(t) + g_o(t)$$

$$g_c(t) = \text{Re}[\bar{g}(t)e^{-j4\pi/3}] + g_o(t) = \text{Re}[\bar{g}_c(t)] + g_o(t) = -\frac{1}{2}g_\alpha(t) - \frac{\sqrt{3}}{2}g_\beta(t) + g_o(t)$$

## Espressioni matriciali

$$\begin{bmatrix} g_\alpha \\ g_\beta \\ g_o \end{bmatrix} = \underline{g}_{\alpha\beta o} = \underline{T}_{abc \rightarrow \alpha\beta o} \underline{g}_{abc} = \underline{T}_{abc \rightarrow \alpha\beta o} \begin{bmatrix} g_a \\ g_b \\ g_c \end{bmatrix}$$

$$\underline{g}_{abc} = \underline{T}_{\alpha\beta o \rightarrow abc} \underline{g}_{\alpha\beta o}$$

$$\underline{T}_{abc \rightarrow \alpha\beta o} = \frac{2}{3} \begin{bmatrix} 1 & -1/2 & -1/2 \\ 0 & \sqrt{3}/2 & -\sqrt{3}/2 \\ 1/2 & 1/2 & 1/2 \end{bmatrix}$$

$$\underline{T}_{\alpha\beta o \rightarrow abc} = \begin{bmatrix} 1 & 0 & 1 \\ -1/2 & \sqrt{3}/2 & 1 \\ -1/2 & -\sqrt{3}/2 & 1 \end{bmatrix} = (\underline{T}_{abc \rightarrow \alpha\beta o})^{-1}$$

$$g_\alpha(t) = \frac{2}{3} \left[ g_a(t) - \frac{g_b(t)}{2} - \frac{g_c(t)}{2} \right]$$

$$g_\beta(t) = \frac{1}{\sqrt{3}} [g_b(t) - g_c(t)]$$

$$g_o(t) = \frac{g_a(t) + g_b(t) + g_c(t)}{3}$$

$$g_a(t) = g_\alpha(t) + g_o(t)$$

$$g_b(t) = -\frac{1}{2} g_\alpha(t) + \frac{\sqrt{3}}{2} g_\beta(t) + g_o(t)$$

$$g_c(t) = -\frac{1}{2} g_\alpha(t) - \frac{\sqrt{3}}{2} g_\beta(t) + g_o(t)$$

## Espressioni matriciali (nel caso in cui non sia di interesse o sia nulla la componente omopolare)

$$\begin{bmatrix} g_\alpha \\ g_\beta \end{bmatrix} = \underline{g}_{\alpha\beta} = \underline{T}_{abc \rightarrow \alpha\beta} \underline{g}_{abc} = \underline{T}_{abc \rightarrow \alpha\beta} \begin{bmatrix} g_a \\ g_b \\ g_c \end{bmatrix}$$

$$\underline{g}_{abc} = \underline{T}_{\alpha\beta o \rightarrow abc} \underline{g}_{\alpha\beta o}$$

$$\underline{T}_{abc \rightarrow \alpha\beta} = \frac{2}{3} \begin{bmatrix} 1 & -1/2 & -1/2 \\ 0 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix}$$

$$\underline{T}_{\alpha\beta \rightarrow abc} = \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix}$$

$$g_\alpha(t) = \frac{2}{3} \left[ g_a(t) - \frac{g_b(t)}{2} - \frac{g_c(t)}{2} \right]$$

$$g_\beta(t) = \frac{1}{\sqrt{3}} [g_b(t) - g_c(t)]$$

$$g_o(t) = \frac{g_a(t) + g_b(t) + g_c(t)}{3}$$

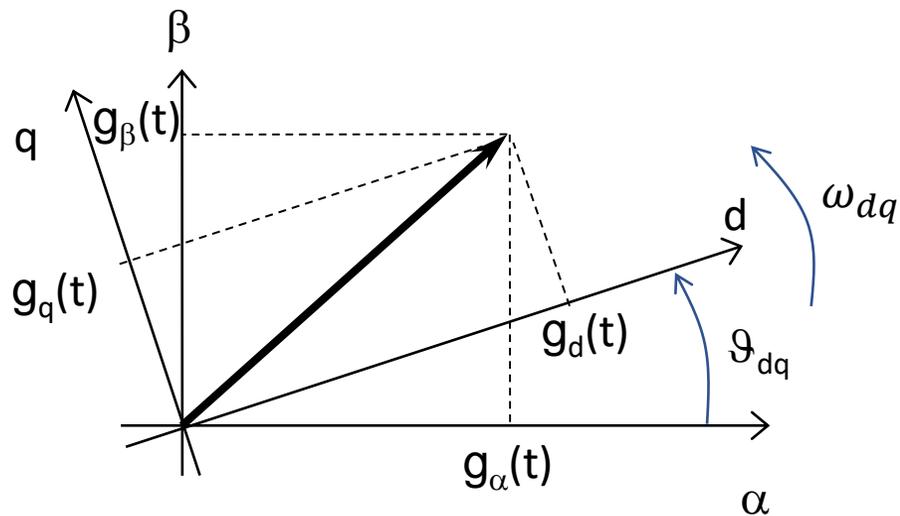
$$g'_a(t) = g_\alpha(t) \cong g_a(t)$$

$$g'_b(t) = -\frac{1}{2} g_\alpha(t) + \frac{\sqrt{3}}{2} g_\beta(t) \cong g_b(t)$$

$$g'_c(t) = -\frac{1}{2} g_\alpha(t) - \frac{\sqrt{3}}{2} g_\beta(t) \cong g_c(t)$$

## Vettore spaziale nel sistema di riferimento rotante (ruotato): assi d-q

$$\vartheta_{dq}(t) = \int_0^t \omega_{dq}(t) dt + \vartheta_{dq}(0)$$



Da dq ad  $\alpha\text{-}\beta$

$$\bar{g}_{\alpha\beta} = e^{j\vartheta_{dq}} \bar{g}_{dq}$$

$$(g_\alpha + jg_\beta) = (\cos\vartheta_{dq} + j\sin\vartheta_{dq})(g_d + jg_q)$$

Da  $\alpha\text{-}\beta$  a dq

$$\bar{g}_{dq} = e^{-j\vartheta_{dq}} \bar{g}_{\alpha\beta}$$

$$(g_d + jg_q) = (\cos\vartheta_{dq} - j\sin\vartheta_{dq})(g_\alpha + jg_\beta)$$

## Espressioni matriciali

$$\begin{bmatrix} g_\alpha \\ g_\beta \end{bmatrix} = \underline{g}_{\alpha\beta} = \underline{T}_{dq \rightarrow \alpha\beta} \underline{g}_{dq} = \underline{T}_{dq \rightarrow \alpha\beta} \begin{bmatrix} g_d \\ g_q \end{bmatrix}$$

$$\underline{g}_{dq} = \underline{T}_{\alpha\beta \rightarrow dq} \underline{g}_{\alpha\beta}$$

$$\underline{T}_{dq \rightarrow \alpha\beta} = \begin{bmatrix} \cos\vartheta_{dq} & -\sin\vartheta_{dq} \\ \sin\vartheta_{dq} & \cos\vartheta_{dq} \end{bmatrix}$$

$$\underline{T}_{\alpha\beta \rightarrow dq} = \begin{bmatrix} \cos\vartheta_{dq} & \sin\vartheta_{dq} \\ -\sin\vartheta_{dq} & \cos\vartheta_{dq} \end{bmatrix} = \underline{(T}_{dq \rightarrow \alpha\beta})^{-1}$$

$$\longrightarrow \underline{(T}_{dq \rightarrow \alpha\beta})^{-1} = \underline{(T}_{dq \rightarrow \alpha\beta})^t$$

Da dq ad  $\alpha\text{-}\beta$

$$\bar{g}_{\alpha\beta} = e^{j\vartheta_{dq}} \bar{g}_{dq}$$

$$(g_\alpha + jg_\beta) = (\cos\vartheta_{dq} + j\sin\vartheta_{dq})(g_d + jg_q)$$

Da  $\alpha\text{-}\beta$  a dq

$$\bar{g}_{dq} = e^{-j\vartheta_{dq}} \bar{g}_{\alpha\beta}$$

$$(g_d + jg_q) = (\cos\vartheta_{dq} - j\sin\vartheta_{dq})(g_\alpha + jg_\beta)$$

## Espressioni matriciali : considerazioni aggiuntive (1)

$$\underline{T}_{dq \rightarrow \alpha\beta} = \begin{bmatrix} \cos\vartheta_{dq} & -\sin\vartheta_{dq} \\ \sin\vartheta_{dq} & \cos\vartheta_{dq} \end{bmatrix} = e^{\underline{J}\vartheta_{dq}} \quad \text{con } \underline{J} = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}$$

Dimostrazione (usando la serie di Taylor)

$$e^{\underline{J}\vartheta_{dq}} = 1 + \underline{J}\vartheta_{dq} + \frac{(\underline{J}\vartheta_{dq})(\underline{J}\vartheta_{dq})}{2} + \dots = \begin{bmatrix} 1 - \vartheta_{dq}^2/2 + \vartheta_{dq}^4/24 - \dots & -(\vartheta_{dq} - \vartheta_{dq}^3/6 + \vartheta_{dq}^5/120 - \dots) \\ \vartheta_{dq} - \vartheta_{dq}^3/6 + \vartheta_{dq}^5/120 - \dots & 1 - \vartheta_{dq}^2/2 + \vartheta_{dq}^4/24 - \dots \end{bmatrix} = \begin{bmatrix} \cos\vartheta_{dq} & -\sin\vartheta_{dq} \\ \sin\vartheta_{dq} & \cos\vartheta_{dq} \end{bmatrix}$$

Proprietà

$$e^{\underline{J}0} = \underline{I} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$e^{\underline{J}(\frac{\pi}{2})} = \underline{J}$$

$$\frac{de^{\underline{J}\vartheta_{dq}(t)}}{dt} = e^{\underline{J}\vartheta_{dq}(t)} \underline{J}\omega_{dq}(t) = \omega_{dq}(t) \underline{J} e^{\underline{J}\vartheta_{dq}(t)}$$

Di norma non vale la proprietà commutativa, ma **qui vale!**

$$\left( e^{j0} = 1 \right.$$

$$e^{j\pi/2} = j$$

$$\left. \frac{de^{j\vartheta_{dq}(t)}}{dt} = e^{j\vartheta_{dq}(t)} j \omega_{dq}(t) = \omega_{dq}(t) j e^{j\vartheta_{dq}(t)} \right)$$

(Per confronto)

## Espressioni matriciali : considerazioni aggiuntive (2)

espressioni matriciali

$$\underline{g}_{\alpha\beta} = e^{\underline{J}\vartheta_{dq}} \underline{g}_{dq}$$

$$\underline{g}_{dq} = e^{-\underline{J}\vartheta_{dq}} \underline{g}_{\alpha\beta}$$

Qui NON VALE la proprietà commutativa.

espressioni complesse

$$\bar{g}_{\alpha\beta} = e^{j\vartheta_{dq}} \bar{g}_{dq}$$

$$\bar{g}_{dq} = e^{-j\vartheta_{dq}} \bar{g}_{\alpha\beta}$$

Qui VALE la proprietà commutativa.

Vale inoltre la seguente proprietà

$$\text{da: } (\underline{T}_{dq \rightarrow \alpha\beta})^{-1} = (\underline{T}_{dq \rightarrow \alpha\beta})^t \quad \longrightarrow \quad (e^{\underline{J}\vartheta_{dq}})^t = (e^{\underline{J}\vartheta_{dq}})^{-1} = e^{-\underline{J}\vartheta_{dq}}$$

# Bilanci energetici (potenza trifase, energia trifase) (1)

In funzione delle grandezze trifase

$$p(t) = u_a(t)i_a(t) + u_b(t)i_b(t) + u_c(t)i_c(t)$$

$$p(t) = \underline{u}_{abc}^t \underline{i}_{abc}$$

che diventa

$$\begin{bmatrix} 3/2 & 0 & 0 \\ 0 & 3/2 & 0 \\ 0 & 0 & 3 \end{bmatrix}$$

$$p(t) = (\underline{T}_{\alpha\beta o \rightarrow abc} \underline{u}_{\alpha\beta o})^t (\underline{T}_{\alpha\beta o \rightarrow abc} \underline{i}_{\alpha\beta o}) = (\underline{u}_{\alpha\beta o}^t \underline{T}_{\alpha\beta o \rightarrow abc}^t) (\underline{T}_{\alpha\beta o \rightarrow abc} \underline{i}_{\alpha\beta o}) = \underline{u}_{\alpha\beta o}^t (\underbrace{\underline{T}_{\alpha\beta o \rightarrow abc}^t \underline{T}_{\alpha\beta o \rightarrow abc}}) \underline{i}_{\alpha\beta o}$$

e dopo aver sviluppato i prodotti matriciali fra le matrici di trasformazione.....

## Bilanci energetici (2)

...la potenza istantanea risulta

$$p(t) = \frac{3}{2} [u_\alpha(t)i_\alpha(t) + u_\beta(t)i_\beta(t)] + 3u_o(t)i_o(t) = \frac{3}{2} [\underline{u}_{\alpha\beta}^t(t) \underline{i}_{\alpha\beta}(t)] + 3u_o(t)i_o(t)$$

Il primo addendo (la parte non dipendente dalle componenti omopolare) vale anche

$$p(t) = \frac{3}{2} [u_\alpha(t)i_\alpha(t) + u_\beta(t)i_\beta(t)] = \frac{3}{2} [\underline{u}_{\alpha\beta}^t(t) \underline{i}_{\alpha\beta}(t)] = \frac{3}{2} [\underline{u}_{dq}^t(t) (\underline{T}_{dq \rightarrow \alpha\beta})^t \underline{T}_{dq \rightarrow \alpha\beta} \underline{i}_{dq}(t)] =$$

$$= \frac{3}{2} [\underline{u}_{dq}^t(t) (\underline{T}_{dq \rightarrow \alpha\beta})^{-1} \underline{T}_{dq \rightarrow \alpha\beta} \underline{i}_{dq}(t)] = \frac{3}{2} [\underline{u}_{dq}^t(t) \underline{i}_{dq}(t)]$$


Le trasformazioni da  $abc$  in  $\alpha\beta$  e  $dq$  non sono conservative per le potenze