



Energy and Buildings

Calculation of a thermal bridge using FEMM 4.2

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Thermal bridge

Definition (ISO 10211)

Part of the building envelope where the otherwise uniform thermal resistance is significantly changed

- by full or partial penetration of the building envelope by **materials** with a different **thermal conductivity**;
- by change in **thickness of the fabric** or difference between **internal and external areas** such as occur at wall/floor/ceiling junctions.

Thermal bridge

Change of thermal transmittance due to a discontinuity in the **materials** or **geometry** of the building envelope



- Additional heat flow has an impact on **energy needs**
- Local decrease of internal surface temperature may cause **condensation** problems in the heating season

Objectives

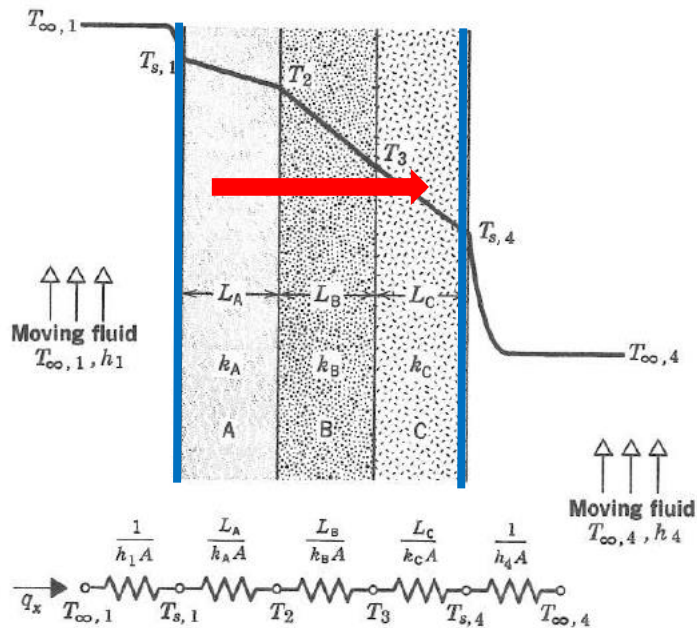
Use a software for the calculation of thermal bridges in building constructions:

1. Calculate additional heat flow in thermal bridges (according to ISO 10211)
2. Assess the risk of surface condensation (according to ISO 13788)

FEMM 4.2 <http://www.femm.info/wiki/Download>

Heat conduction in solids

Analytical solution for 1D steady-state problem on a composite wall



Equivalent thermal circuit for a composite wall
(Incropera & DeWitt, 1981)

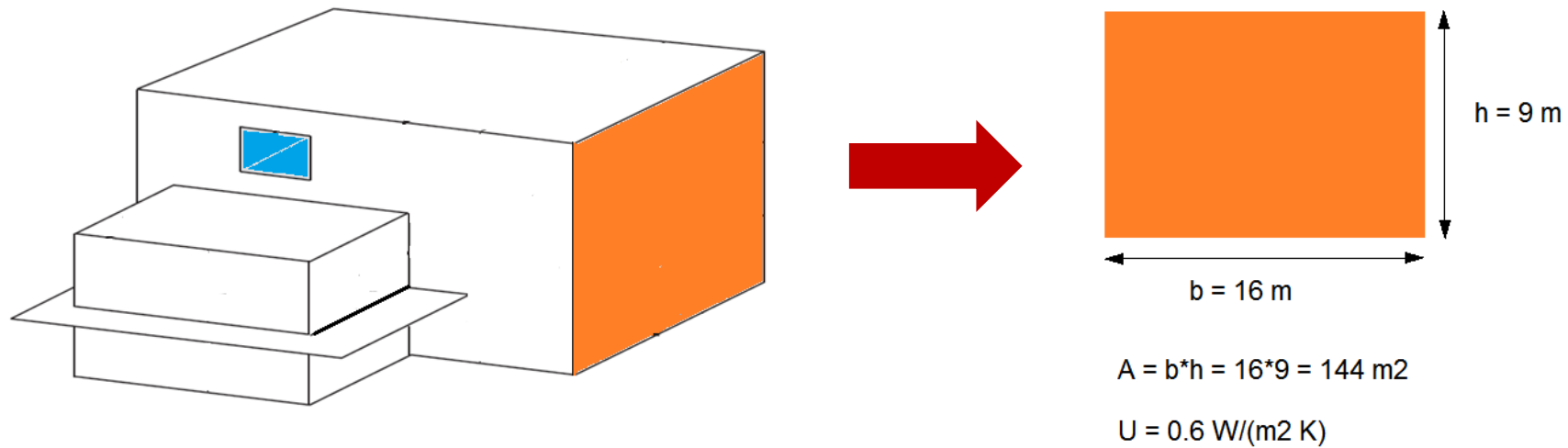
$$\frac{\partial}{\partial x} \left(k_x \frac{\partial T}{\partial x} \right) = 0$$

ELECTRICAL ANALOGY (1)

Fix temperature difference $(T_1 - T_2) \rightarrow$
find heat flow q_x

$$q_x = \frac{(T_1 - T_2)}{\sum_i R_i}$$

Heat loss coefficient



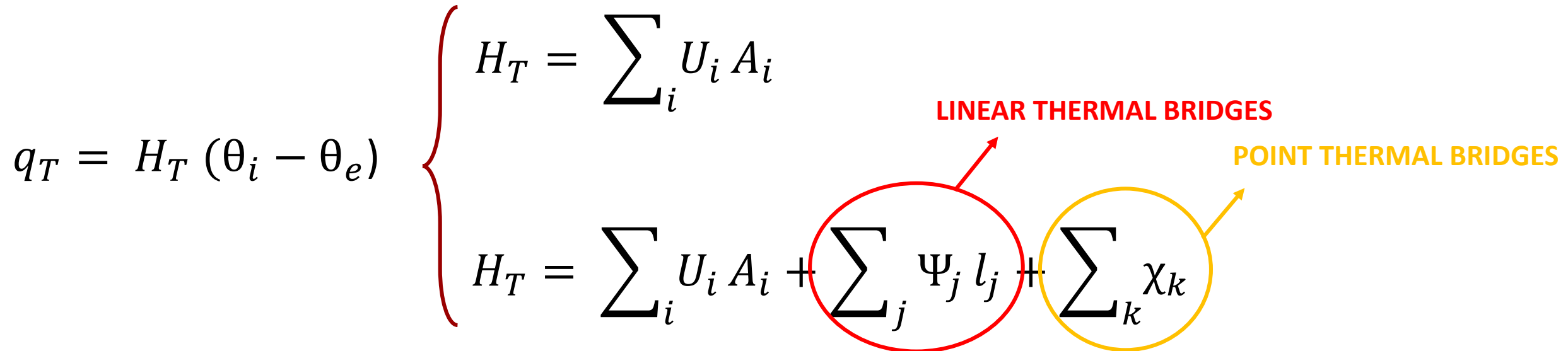
$$\textcircled{q_T} = H_T (\theta_i - \theta_e) \quad \dashrightarrow \quad H_T = \sum_i U_i A_i$$

Transmission heat transfer coefficient

$$q_T = H_T (\theta_i - \theta_e) \left\{ \begin{array}{l} H_T = \sum_i U_i A_i \\ H_T = \sum_i U_i A_i + \sum_j \Psi_j l_j + \sum_k \chi_k \end{array} \right.$$

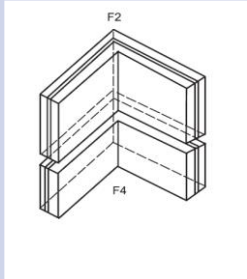
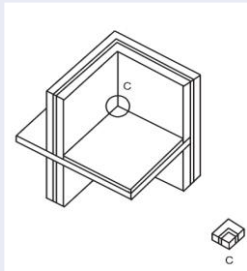
LINEAR THERMAL BRIDGES

POINT THERMAL BRIDGES



The diagram illustrates the calculation of the transmission heat transfer coefficient H_T . It shows two equations for H_T grouped by a large red curly brace. The first equation is $H_T = \sum_i U_i A_i$. The second equation is $H_T = \sum_i U_i A_i + \sum_j \Psi_j l_j + \sum_k \chi_k$. The term $\sum_j \Psi_j l_j$ is circled in red, with a red arrow pointing to the text "LINEAR THERMAL BRIDGES". The term $\sum_k \chi_k$ is circled in yellow, with a yellow arrow pointing to the text "POINT THERMAL BRIDGES".

Calculation method of ISO 10211

Geometrical model	Example	Method
2D		<p>Linear thermal transmittance, Ψ (W/(m K)) Thermal coupling coefficient from 2D calculation, L_{2D} (W/(m K))</p> $\Psi = L_{2D} - \sum_{j=1}^{N_j} U_j l_j$
3D		<p>Point thermal transmittance, χ (W/K) Thermal coupling coefficient from 3D calculation, L_{3D} (W/K)</p> $\chi = L_{3D} - \sum_{i=1}^{N_i} U_i A_i - \sum_{j=1}^{N_j} \Psi_j l_j$

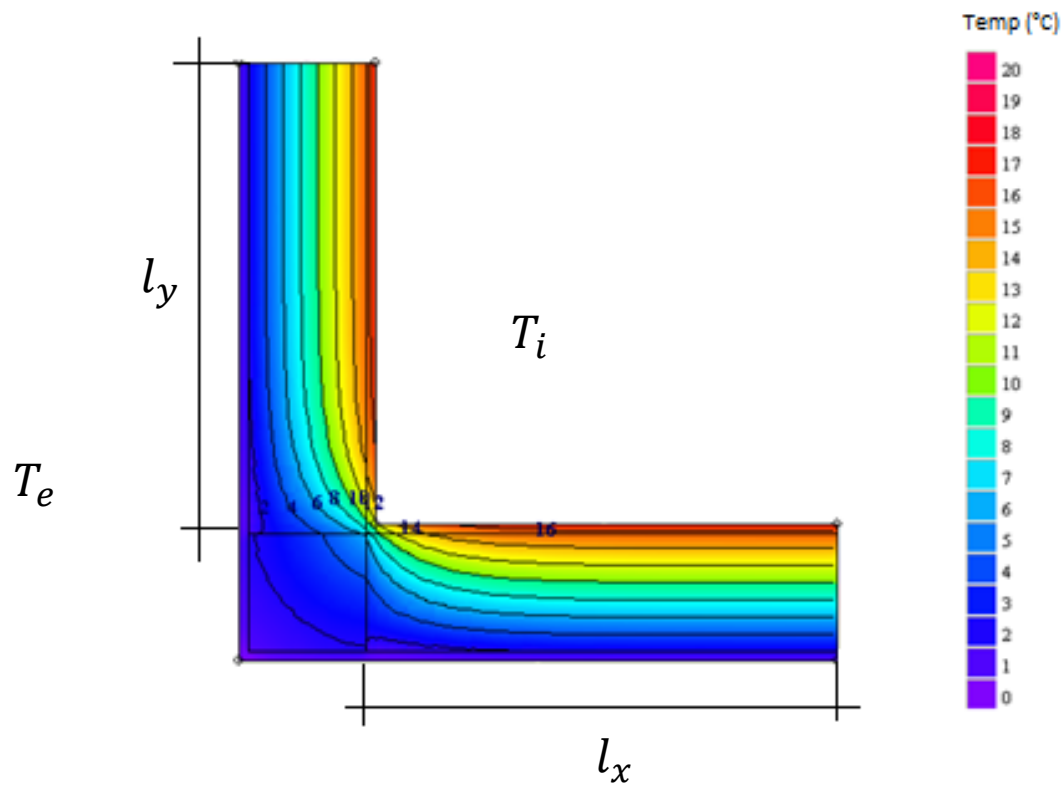
Calculation method of ISO 10211

Thermal coupling coefficient

The thermal coupling coefficient (L_{2D} or L_{3D}) is heat flow rate per temperature difference between two environments which are thermally connected by the construction under consideration.

$$L_{2D} = \frac{Q_{ie}}{l(T_i - T_e)} \left[\frac{W}{m K} \right]$$

Calculation of the linear thermal transmittance

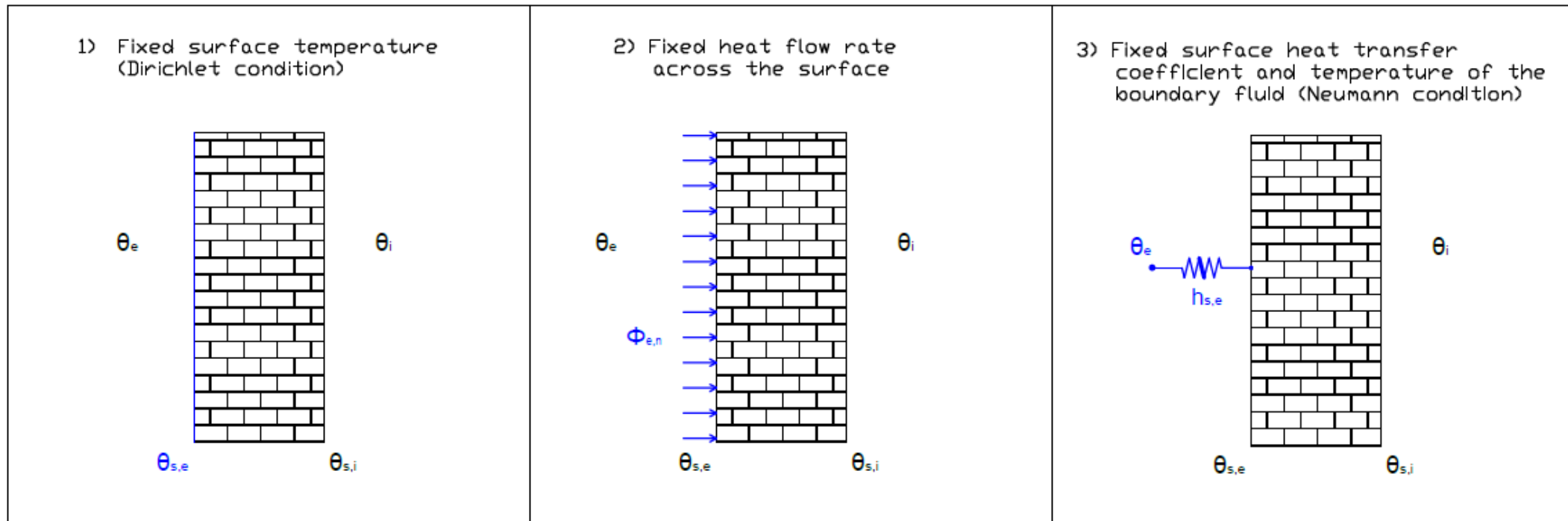


1. Evaluate **temperature distribution** with 2D heat conduction calculation software
2. Integrate temperature difference over normal surface to get the heat flow rate q_{ie} and to calculate the thermal coupling coefficient L_{2D}
3. Calculate the linear thermal transmittance according to Standard

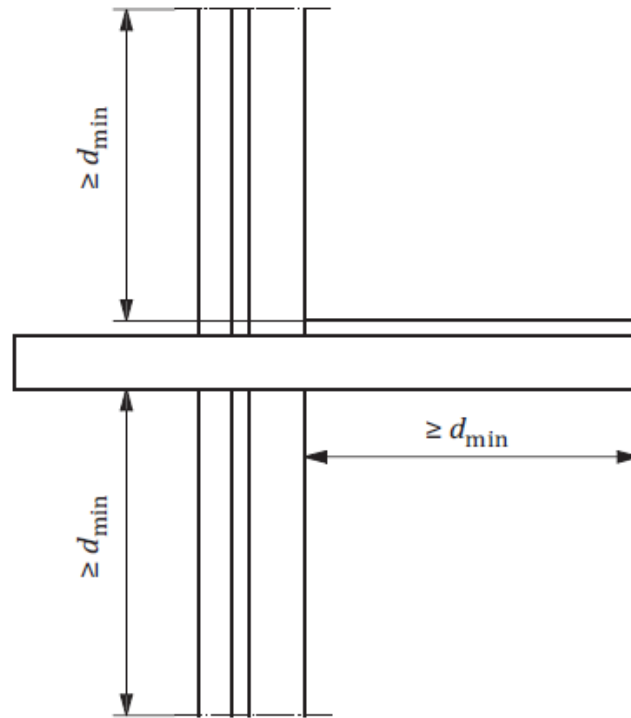
$$\Psi = L_{2D} - (U_x l_x + U_y l_y)$$

Calculation method of ISO 10211

Types of boundary conditions



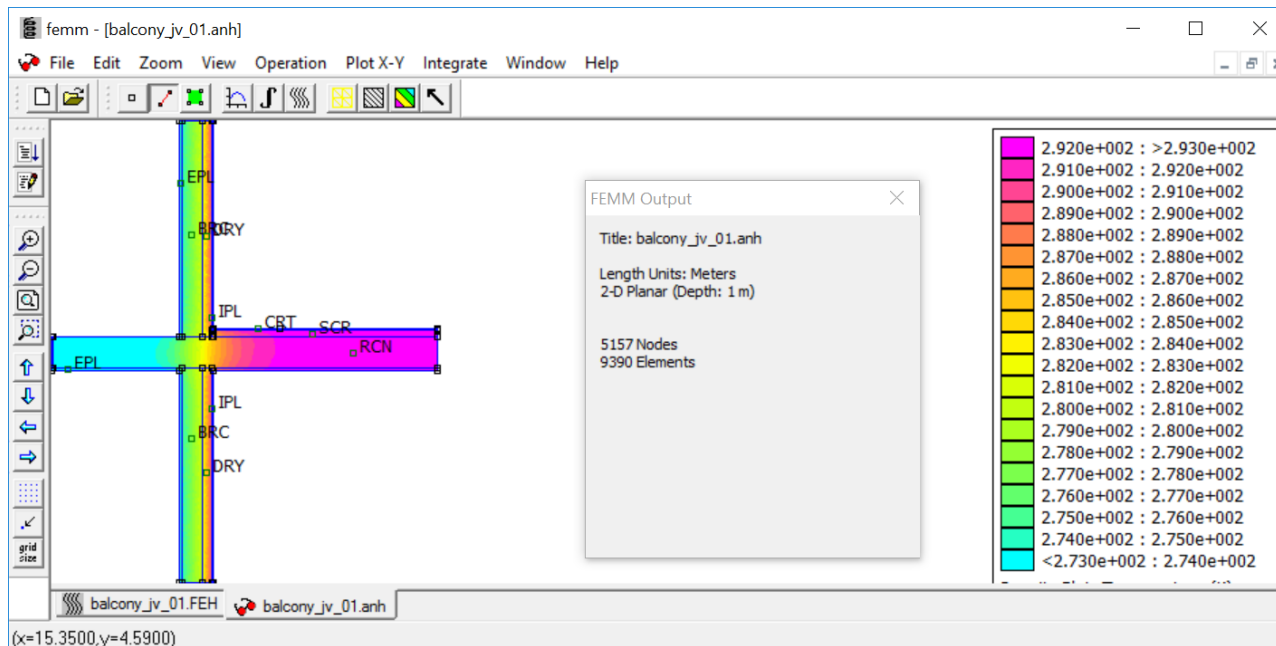
Calculation method of ISO 10211



Calculation of the linear thermal transmittance

Minimum distances of cut-off planes for 2D geometrical models is a function of envelope thickness according to the Standard

FEMM 4.2

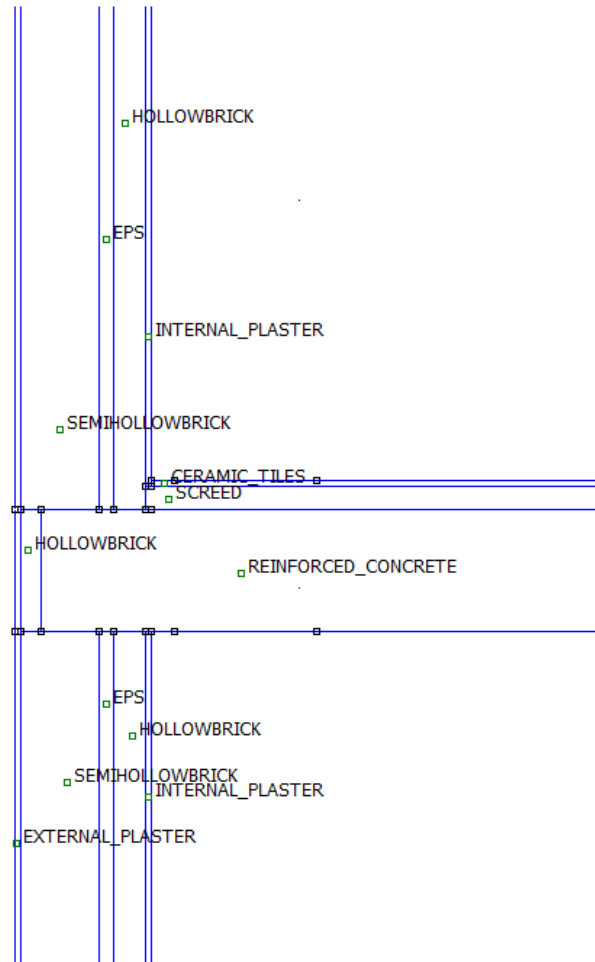


The FEMM software is a **finite element** package for solving **2D planar** and axisymmetric magnetic, electrostatic, **steady-state heat conduction**, and current flow **problems**.

Calculation method of ISO 10211

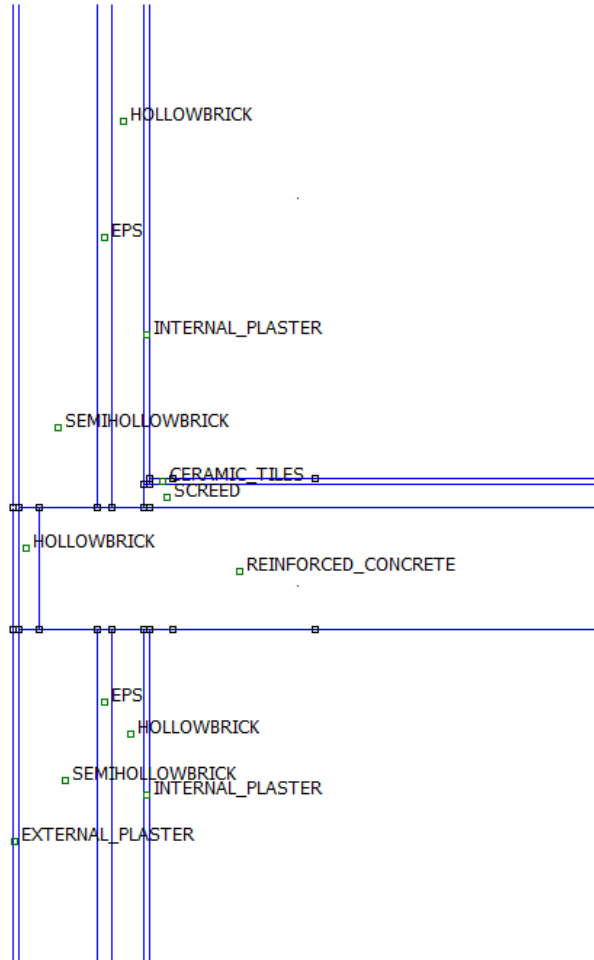
Steps for the calculation of the thermal bridge with FEMM 4.2:

1. Import geometry from a .dxf file
2. Set material properties for each building component
3. Set boundary conditions
4. Create a mesh to discretize the domain
5. Run the FEM solver to calculate the temperature distribution
6. Integrate temperature difference over normal surface
7. Calculate L_{2D} , ψ and minimum surface temperature

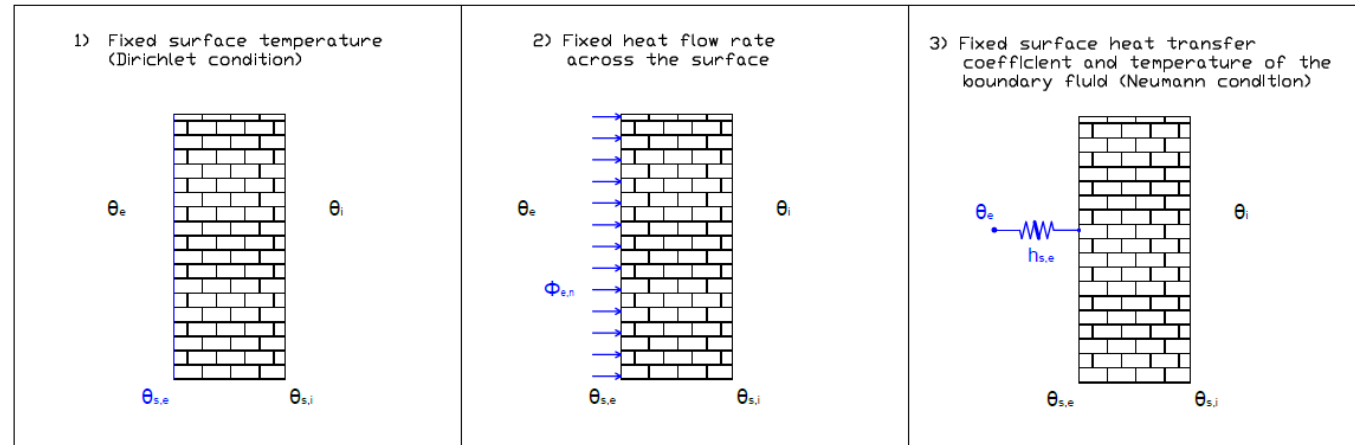


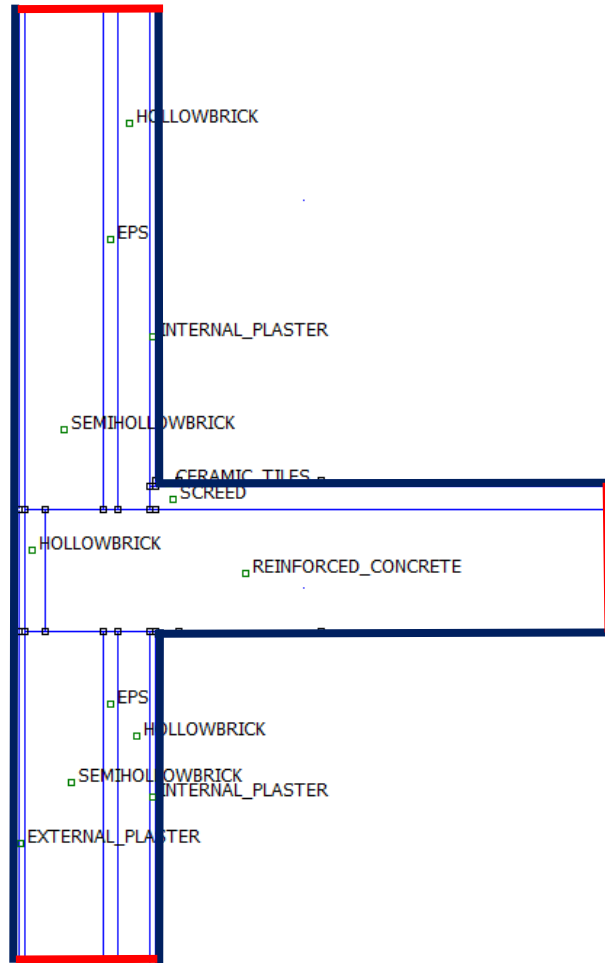
Intermediate floor junction

Material (eng)	Material (it)	Thermal conductivity k [W/(m K)]	Volumetric heat capacity c [MJ/(m ³ K)]
Internal plaster	Intonaco interno (calce e gesso)	0.70	1.26
External plaster	Intonaco esterno (calce e cemento)	1.00	1.51
Reinforced concrete	Cemento armato	2.30	2.02
Screed	Massetto (calcestruzzo alleggerito con argilla espansa)	0.45	0.92
Semi-hollow bricks	Laterizio semipieno	0.70	1.01
Hollow bricks	Tramezza in laterizio	0.36	0.92
Ceramic tiles	Piastrelle di ceramica	1.20	1.68
Polystyrene (EPS)	Polistirene espanso (EPS)	0.04	0.05

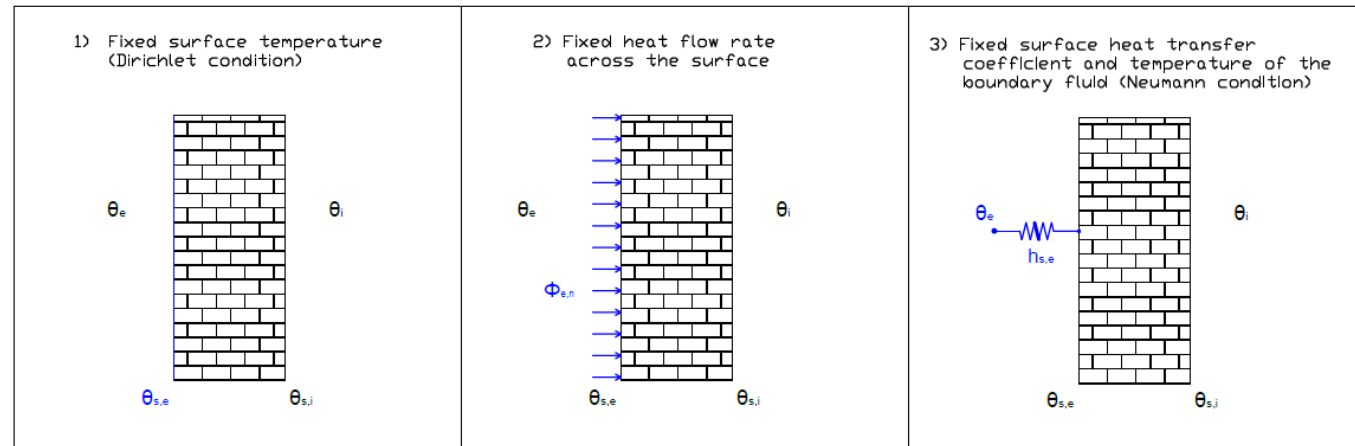


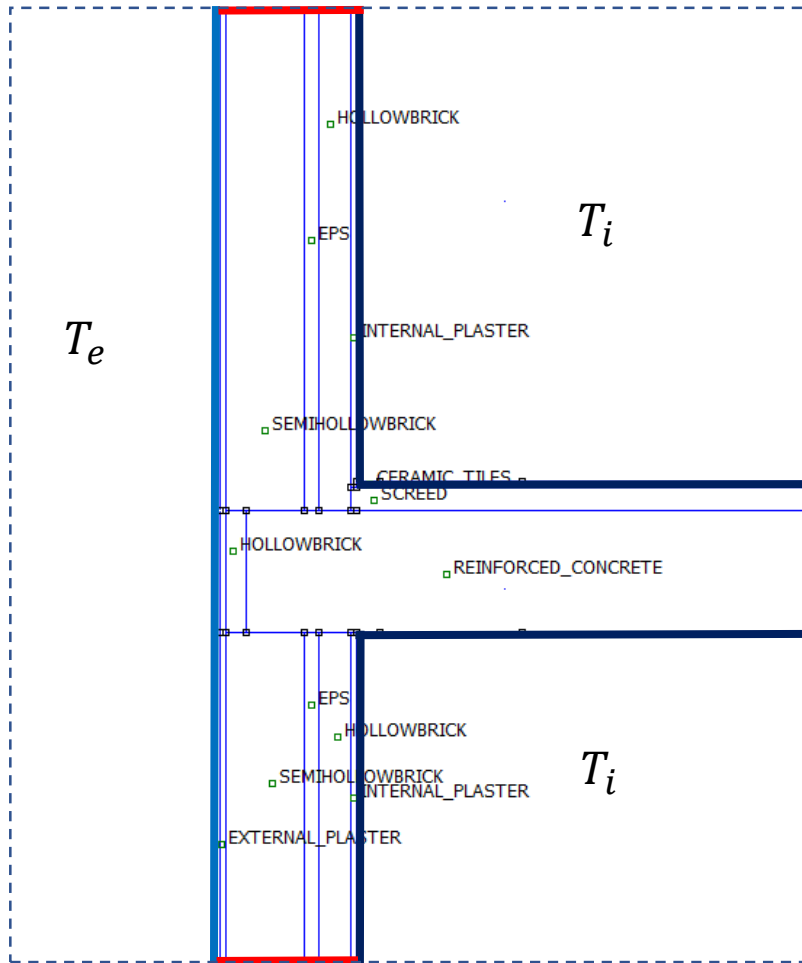
- Boundary condition of the III type
 $h_{si} = 8 \text{ W/(m}^2 \text{ K)}$
 $h_{se} = 25 \text{ W/(m}^2 \text{ K)}$
- Adiabatic surface ($q = 0$)
 Boundary condition of the II type





- Boundary condition of the III type
 $h_{si} = 8 \text{ W/(m}^2 \text{ K)}$
 $h_{se} = 25 \text{ W/(m}^2 \text{ K)}$
- Adiabatic surface ($q = 0$)
 Boundary condition of the II type





Boundary condition of the II type
 — Adiabatic surface ($q = 0$)

Boundary conditions of the III type
 — $h_{si} = 8 \text{ W}/(\text{m}^2 \text{ K}), T_i = 20^\circ\text{C}$
 — $h_{se} = 25 \text{ W}/(\text{m}^2 \text{ K}), T_e = 0^\circ\text{C}$