

Calculation procedure for surface condensation

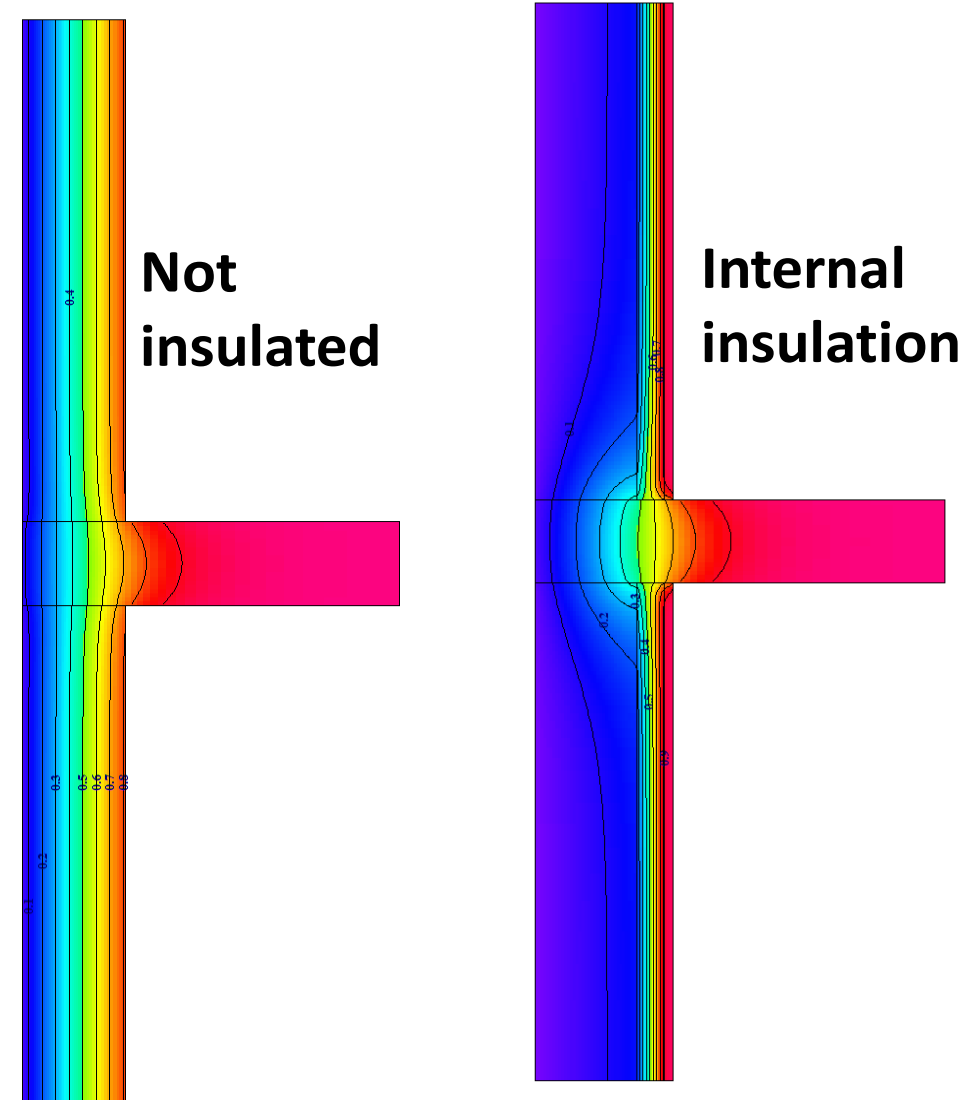
Output of the 2D calculation

The output of the 2D simulation is the temperature factor f_{RSi} .

The picture shows a thermal bridge due to the presence of different materials.

$$f_{RSi} = 0.74$$

How can we correlate this minimum local temperature with the surface condensation problems?

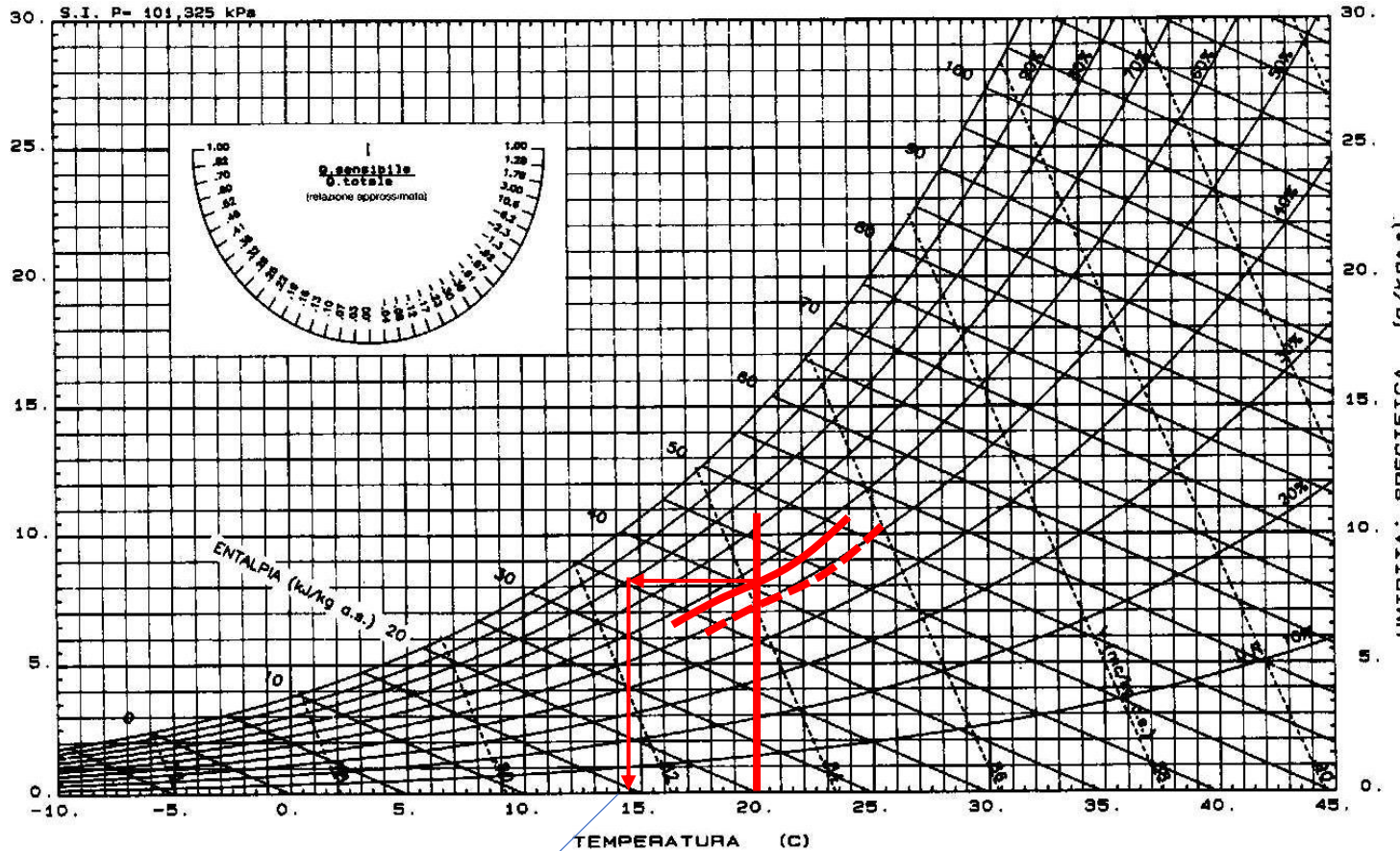


$$f_{RSi} = 0.74 = (\theta_{si} - \theta_e) / (\theta_i - \theta_e)$$

Let's consider Milan in January with $\theta_{si} = 1.7^\circ\text{C}$

$$\theta_{si} = \theta_e + f_{RSi} * (\theta_i - \theta_e)$$

$$\theta_{si} = 1.7 + 0.74 * (20 - 1.7) = 15.2^\circ\text{C}$$



$$\theta_{si,min} = 14.5^\circ\text{C}$$

$$\theta_{si} > \theta_{si,min}$$

Condensation does not occur

- Two main observations:
- 1) Need to evaluate the indoor conditions
 - 2) Need for calculation procedure

ISO EN 13788

Example 1 – Calculation of the temperature factor – Use of the indoor humidity classes - UNI EN ISO 13788


Calculation of f_{RSi} for January. Location: Milan (climatic data UNI 10349)

$$\theta_e = 1.7^\circ\text{C}; p_v = 590 \text{ Pa}$$

$$\theta_i = 20^\circ\text{C}$$

based on UNI EN ISO 13788

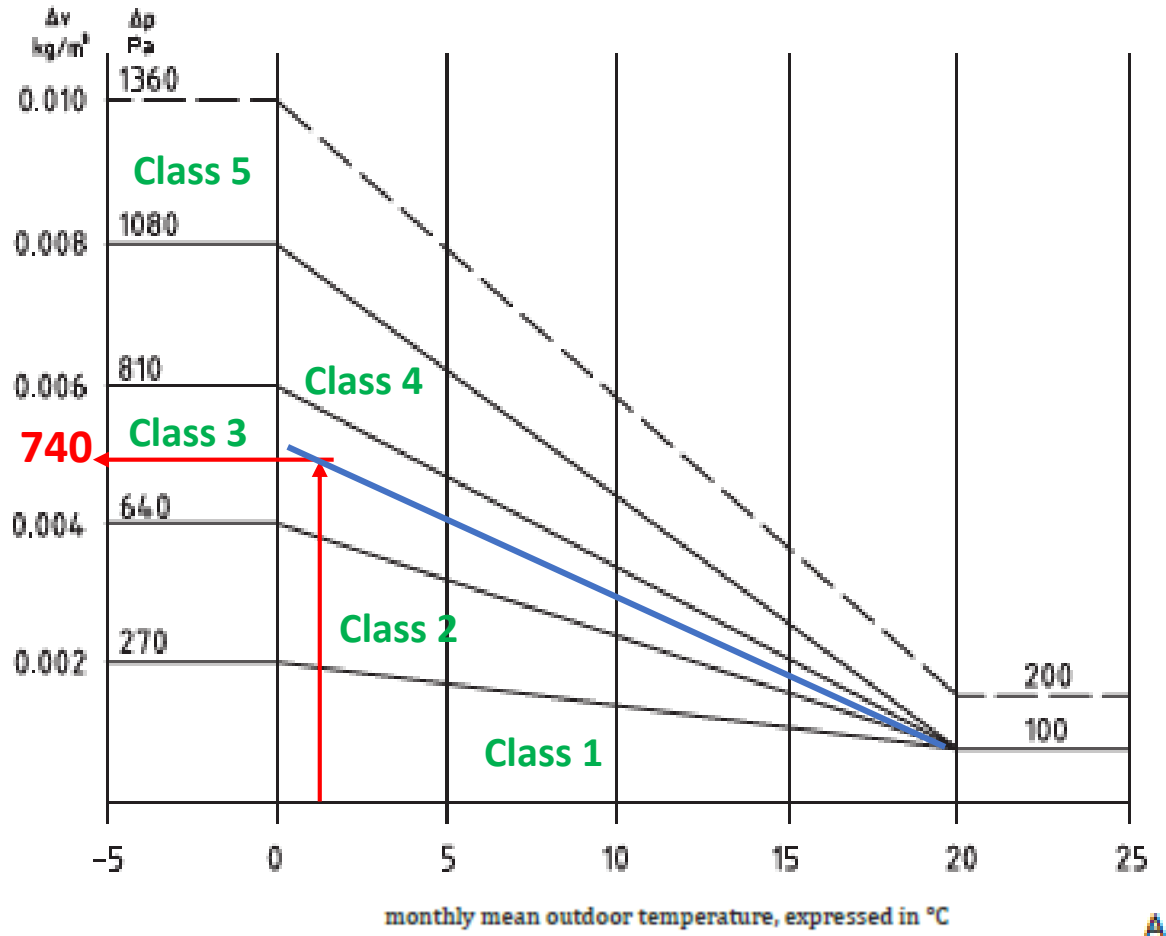
$$p_{\text{sat}} = 610,5 e^{\frac{17,269 \theta}{237,3 + \theta}} \quad \text{per } \theta \geq 0^\circ\text{C}$$



Calculation of $p_{\text{sat}}(\theta_e) = 690 \text{ Pa}$

$$\phi_e = 85.6\%$$

Calculation of the indoor pressure p_v (considering Δp for dwellings with low vapour production, class 3/4)



Considering Δp and the safety factor 1.1 according to UNI EN ISO 13788 the indoor pressure p_v :

$$p_i = p_e + \Delta p = 590 + 740 * 1.1 = 1404 \text{ Pa}$$

Minimum acceptable value for the saturation pressure and minimum surface temperature referred to local condition $\varphi_{si}=0.8$

$$p_{\text{sat}}(\theta_{si}) = p_i / 0.8 = 1404 / 0.8 = 1755 \text{ Pa} \rightarrow \theta_{\text{Si,min}} = 15.5^\circ\text{C}$$

$$\theta = \frac{237,3 \log_e\left(\frac{p_{\text{sat}}}{610,5}\right)}{17,269 - \log_e\left(\frac{p_{\text{sat}}}{610,5}\right)} \quad \text{per } p_{\text{sat}} \geq 610,5 \text{ Pa}$$

Calculation of the minimum temperature factor:

$$f_{\text{RSi,min}} = (\theta_{\text{Si,min}} - \theta_e) / (\theta_i - \theta_e) = (15.5 - 1.7) / (20 - 1.7) = \underline{\underline{0.754}}$$

Example 2 – Calculation of the temperature factor – Use of constant indoor relative humidity - UNI EN ISO 13788

Calculation of f_{RSi} for January. Location: Milan (climatic data UNI 10349)


$$\theta_e = 1.7^\circ\text{C}; p_v = 590 \text{ Pa}$$

$$\theta_i = 20^\circ\text{C}; \phi_i = 50\%$$

based on UNI EN ISO 13788

$$p_{\text{sat}} = 610,5 e^{\frac{17,269 \theta}{237,3 + \theta}}$$

per $\theta \geq 0^\circ\text{C}$


$$\text{Calculation of } p_{\text{sat}}(\theta_i) = 2337 \text{ Pa}$$

Calculation of indoor partial vapour pressure (RH + 0.05 according to UNI EN ISO 13788):

$$p_i = \phi_i p_{\text{sat}}(\theta_i) = 0.55 * 2337 = 1285 \text{ Pa}$$

Minimum acceptable value for the saturation pressure and minimum surface temperature referred to local condition $\varphi_{si}=0.8$

$$p_{\text{sat}}(\theta_{si}) = p_i / 0.8 = 1285 / 0.8 = 1606.3 \text{ Pa} \rightarrow \theta_{\text{Si,min}} = 14.08^\circ\text{C}$$

$$\theta = \frac{237,3 \log_e\left(\frac{p_{\text{sat}}}{610,5}\right)}{17,269 - \log_e\left(\frac{p_{\text{sat}}}{610,5}\right)}$$

per $p_{\text{sat}} \geq 610,5 \text{ Pa}$

Calculation of the minimum temperature factor:

$$f_{\text{RSi,min}} = (\theta_{\text{Si,min}} - \theta_e) / (\theta_i - \theta_e) = (14.08 - 1.7) / (20 - 1.7) = \underline{\underline{0.677}}$$

